

GRACE Mission

***GRACE Mission:
Architecture of the Flight
Segment***

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GRACE Mission Principles

Focus

- "Do one thing. Do it well."
- "Chose an objective that is worth pursuing"

Balance

- "Technology without economics is not engineering"

Risk Containment

- "Don't stretch the limits of hardware performance"

GRACE Mission Balance

- **Minimizing Total Cost**

- Total Cost = $\sum(C_1+C_2+C_3 \dots\dots\dots +C_k)$
- For a given level of performance, Total Cost is minimum if
 - $\partial \text{Perf}/\partial C_1 = \partial \text{Perf}/\partial C_2 = \partial \text{Perf}/\partial C_3 \dots\dots\dots = \partial \text{Perf}/\partial C_k$
- Cost functions are very non-linear and not well known
 - Pushing technology is very costly
 - Doing things for the first time is very costly

- **Line Item Cost = (Fixed Cost) + n x (Unit Cost)**

- GRACE Satellite Subcontract
 - Fixed cost = \$11 M
 - Unit cost = \$12 M / satellite
 - Better thermal control = \$0.06 M total
- Build identical units.
 - Lower total Cost and fewer spares

GRACE Mission Focus

Heritage Gravity Missions all carried a Magnetometer

- NASA's Gravity Research Mission (GRM) proposal - died 1985
- ESA's Aristoteles proposal - died 1990 when NASA pulled out
- NASA-GSFC's GAMES proposal died 1994
- GFZ-Potsdam's CHAMP launched 2000

Heritage Gravity Missions Emphasized Spatial Resolution

- GRM proposed to fly at an altitude of 156 to 170 km
- Aristoteles proposed to fly at an altitude of 200 km

GRACE Mission

Competing Objectives

- **Orbit Design**
 - Magnetic field missions prefer an inclination of 85 degrees
 - Gravity mission prefer an inclination of:
 - First choice - near 90 degrees
 - Second choice - sun-synchronous orbit at 97 degrees
- **Structural Stability**
 - Magnetometers want to be located on a long boom
 - 1 nano-Tesla
 - A satellite for a Gravity Mission needs to be very stable
 - 1 μm @ 2x per orbit, or $5\text{E}-12$ m/s² - .0002 to .04 Hz
- **Root Cause of the Problem: Organizational**
 - Funding for gravity missions came NASA's Geo-potential Fields Program Office

GRACE Mission
The Seminal SST Gravity Mission

Milo Wolff, MIT-SAO - JGR, Vol.,74, No. 22, Oct. 1969

- **Two geometrically identical satellites**
- **Equipped to measure relative velocity**

$$\Delta \mathbf{U} = \mathbf{V}_{\text{mean orbital}} \times \Delta \mathbf{V}_{\text{along track}}$$

- **200-km separation - Altitude \geq separation**
- **USO + Transponded RF signal, or Laser doppler system**
- **Doppler (i.e. $\Delta \mathbf{V}_{\text{along track}}$) sampled every 10 seconds**
- **Store and forward data to the ground**
- **Non-gravitational forces controlled by careful design and accounted for by modeling**

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GRACE - How it Works

Microwave Link

Tracking Phase - Range change

24 & 32-GHz - Ionosphere

Dual One-way - Clocks

GPS

Relative Clocks

Location

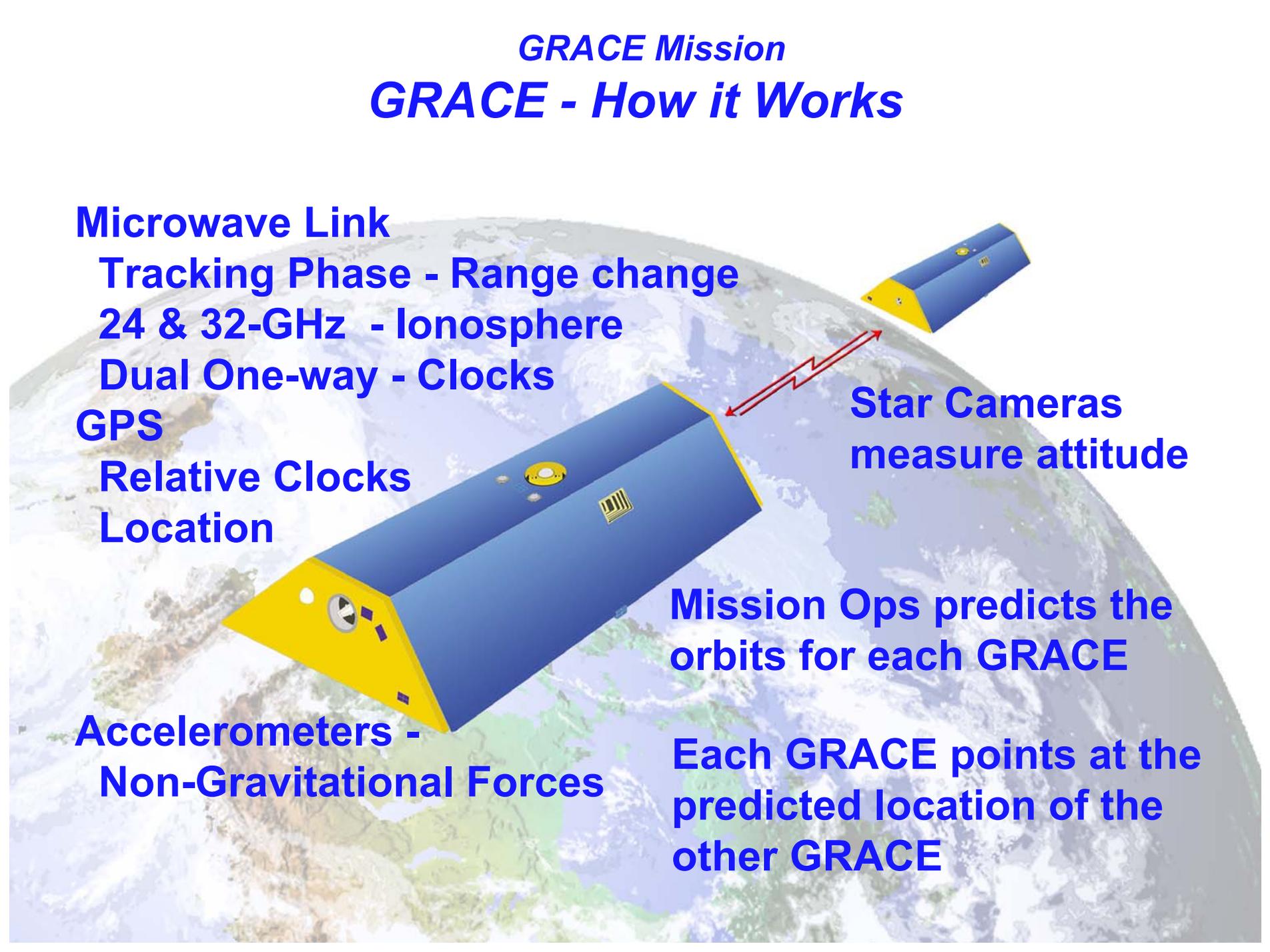
**Accelerometers -
Non-Gravitational Forces**



**Star Cameras
measure attitude**

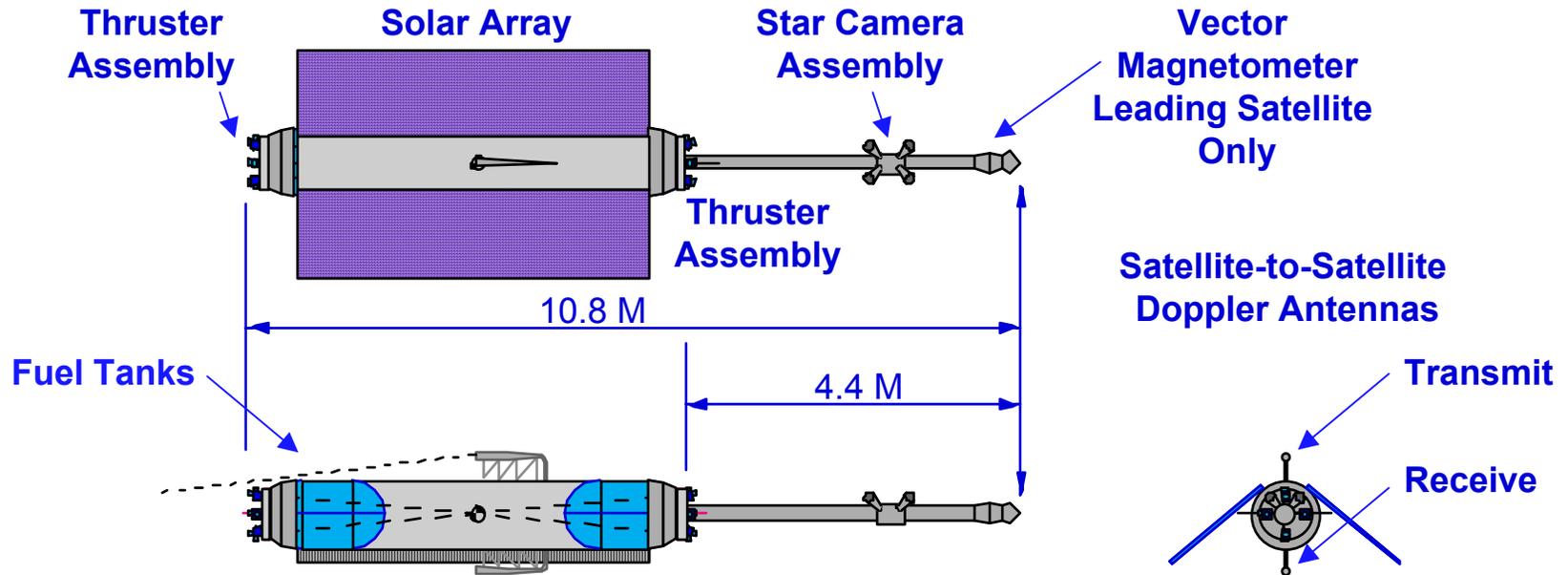
**Mission Ops predicts the
orbits for each GRACE**

**Each GRACE points at the
predicted location of the
other GRACE**



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Gravity Research Mission -1985



Unfriendly Features

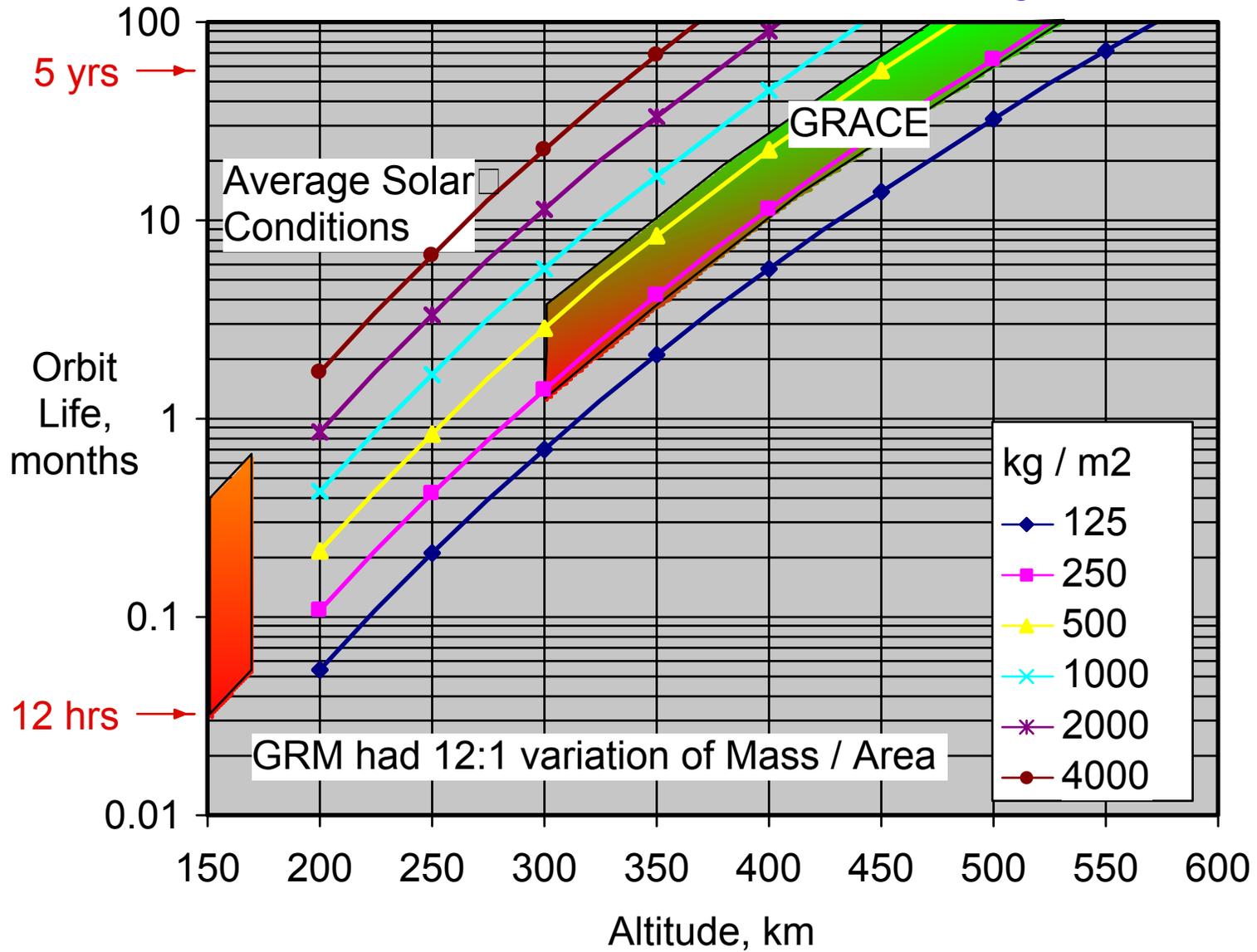
- 1200 kg of Hydrazine Fuel
- Flexible Boom & Solar Arrays
- Multipath on the SST RF link

Challenges

- No feasible operational safe mode
- Continuous Drag Compensation
- Time synchronization

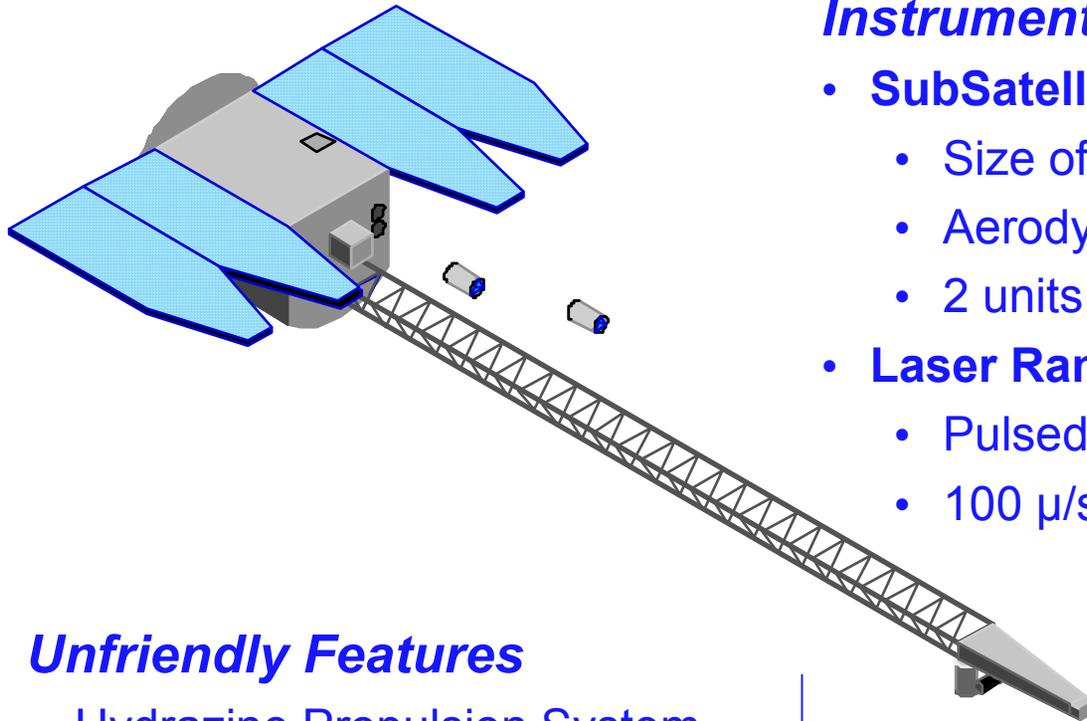
Dual One-Way Ranging Concept Developed at APL!

GRACE Mission Orbit Life & Mission Safety



GRACE Mission

GA \square MES - 1992



Instrumentation Concept

- **SubSatellite Retro Reflectors**
 - Size of a Soda Can
 - Aerodynamically stabilized
 - 2 units released sequentially
- **Laser Ranging System**
 - Pulsed at 2-GHz rate
 - 100 μ /s range rate

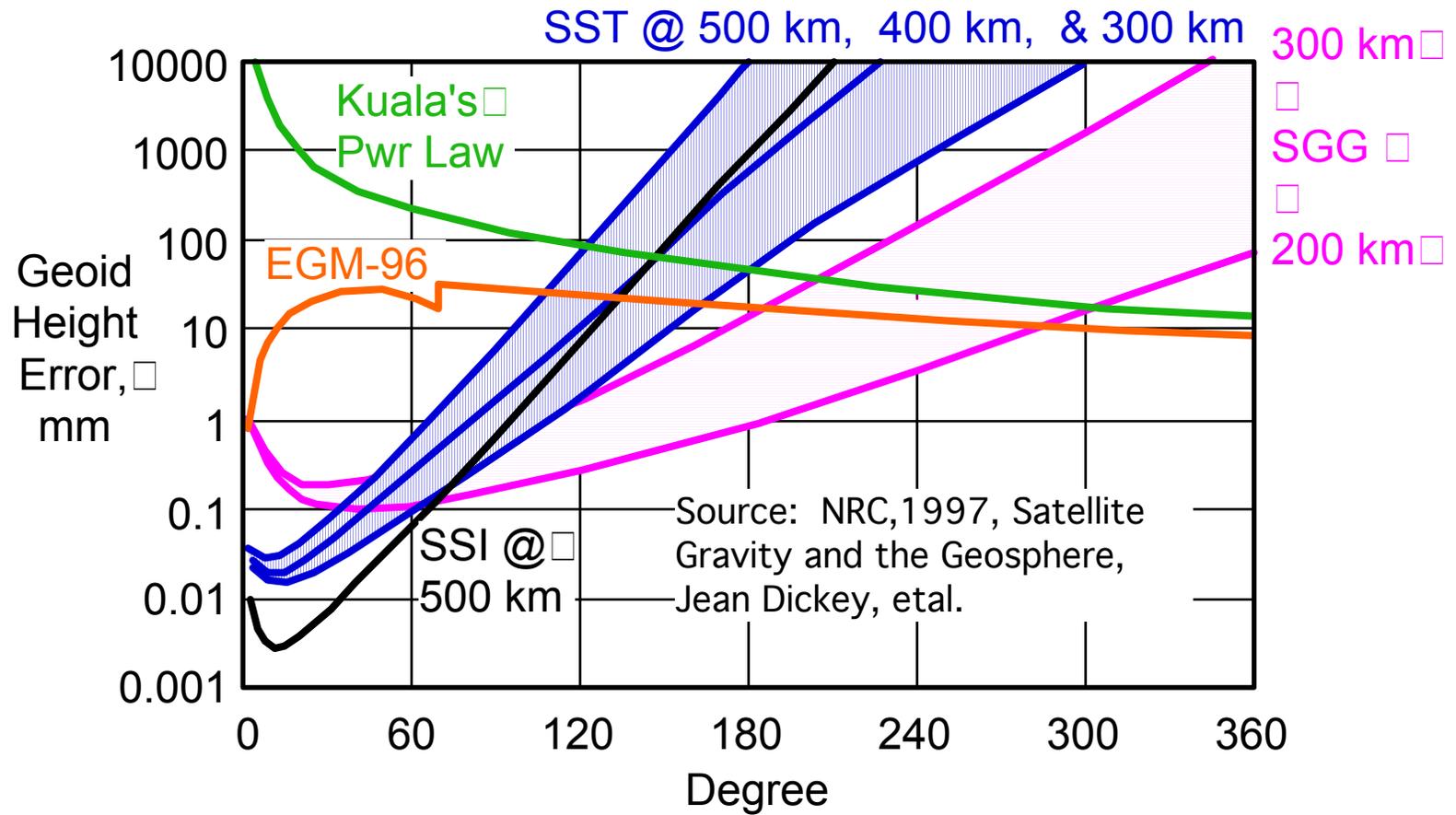
Unfriendly Features

- Hydrazine Propulsion System
- Flexible 6-M boom
- Flexible Solar Arrays
- Uncontrolled Non-gravitational forces - aerodynamic

Challenges

- Acquisition & tracking by the laser ranging telescope
- Sub-satellite aerodynamic stability

GRACE Mission Competition vs. SST (Before GRACE)

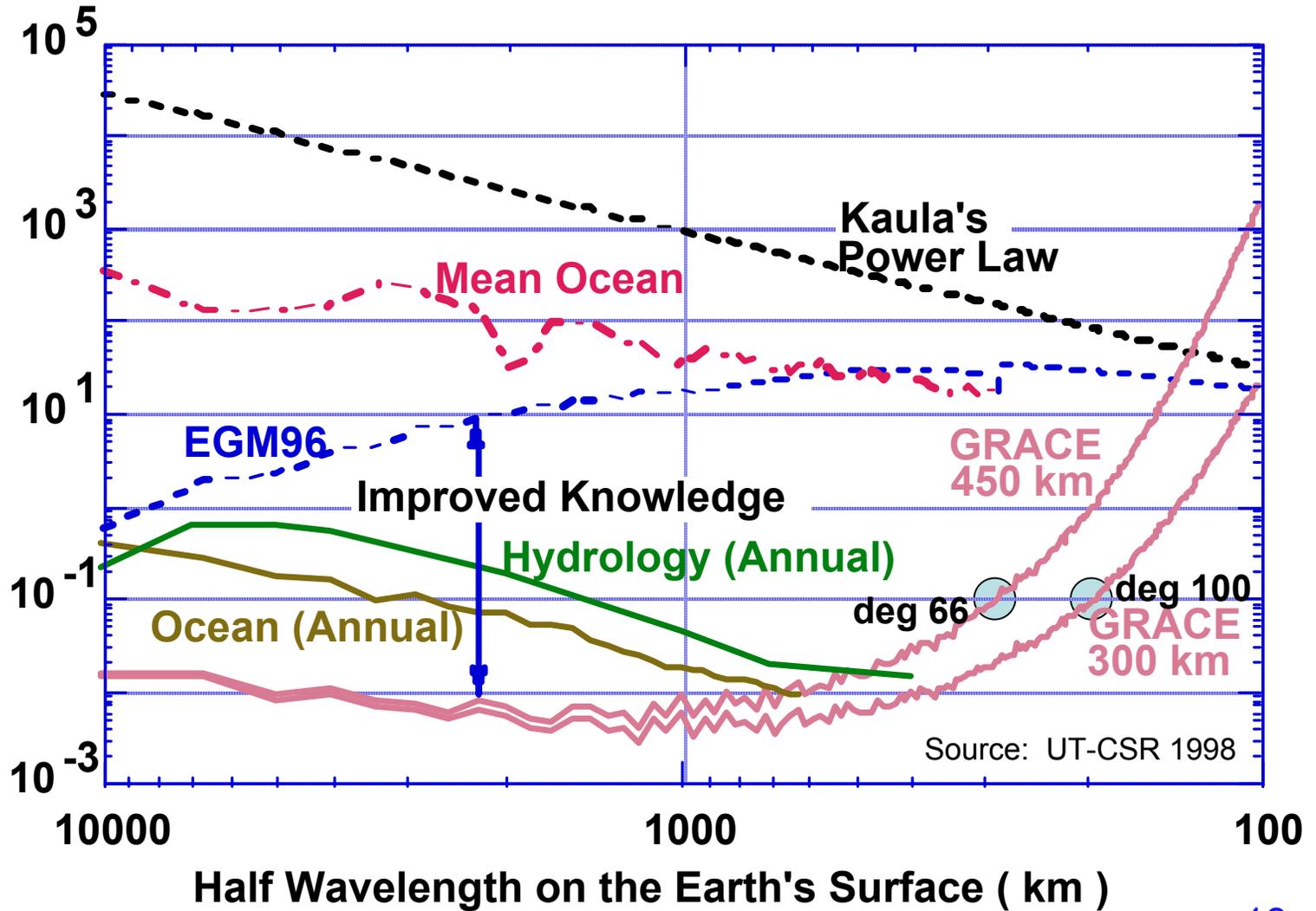


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Listen for Simple Truths

- **Minimum Science Mission Objective - A moving target**
 - Oceanography base
 - 1994 Geoid with 5-cm accuracy cumulative to degree 50
 - 1996 Geoid with 0.5-cm accuracy to degree 50
- **Victor Zlotnicki casually commented "I wouldn't compromise the accuracy of a single low-degree term in order to improve the accuracy of the high-degree terms."**
 - Our response was to develop performance specifications for J2 - usually ignored by predecessors
- **Labrecque pushed the idea of using gravity to measure time-varying geophysical parameters - Richard Gross, B. Chao et al., - "low-degree and order terms were significant"**
- **Brooks Thomas applied signal filter theory to the problem and showed how to improve SST performance @ all scales**

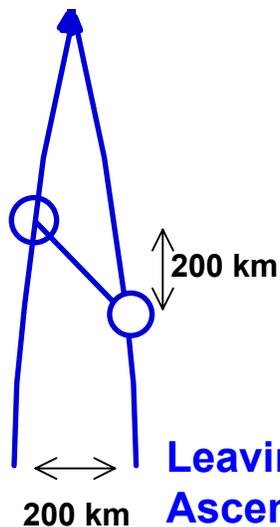
GRACE Mission Focus on the Long Wavelength



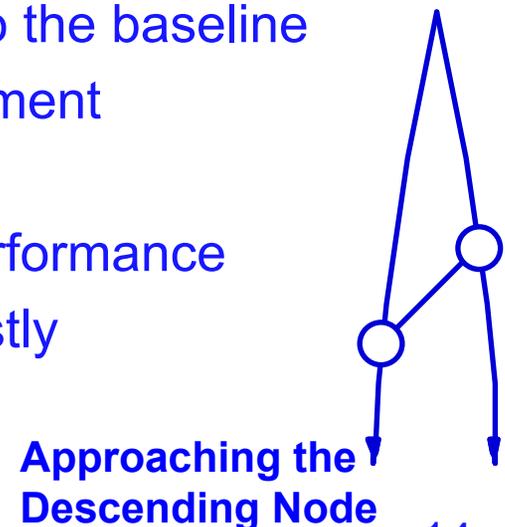
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Abandoned Orbit Design

- **Baseline Co-planar Orbit has one drawback**
 - The partial derivative of the $m=n$ terms of the spherical harmonics are \sim zero for the baseline co-planar, polar, orbit
- **Option for improvement**
 - Offset the LAN's of the twin satellites
 - 40-km offset: Marginal improvement
 - Drag & control penalty similar to the baseline
 - 200-km offset: Significant improvement
 - Drag penalty is high
 - Exceeded out-of plane ACC performance
 - The plane change would be costly



Leaving the
Ascending Node



Approaching the
Descending Node

Impact of the Advanced Digital Filtering

Higher Data Rate for ACC & K-Band data

- Brooks wanted 50 Hz
- Compromised at 10 Hz
- Cost: \$0.0

Attitude Control Pointing

- ≤ 1 mr not good enough
- ≤ 0.5 mr needed
- Cost uncertain

Control on the PSD of the noise from attitude control

- 20-mN thrusters too strong
- 10-mN thrusters needed
- Cost: \$ 0.0 (available)

Center of Mass Control

- ≤ 500 microns not good enough
- ≤ 100 microns needed
- Cost: \$2,000,000 for on-orbit adjustment
- Cost \$50,000 for tank valving

Accelerometer Performance

- $10E-9$ $ms^{-2}Hz^{-1/2}$ no longer good enough
- $10E-10$ needed
- Cost: \$ 0.0 (available)

Digital Filtering the data by 335

- Incremental Cost: Worth it!

GRACE Mission Limiting Error Sources

[Spectral Noise Density]^{1/2}

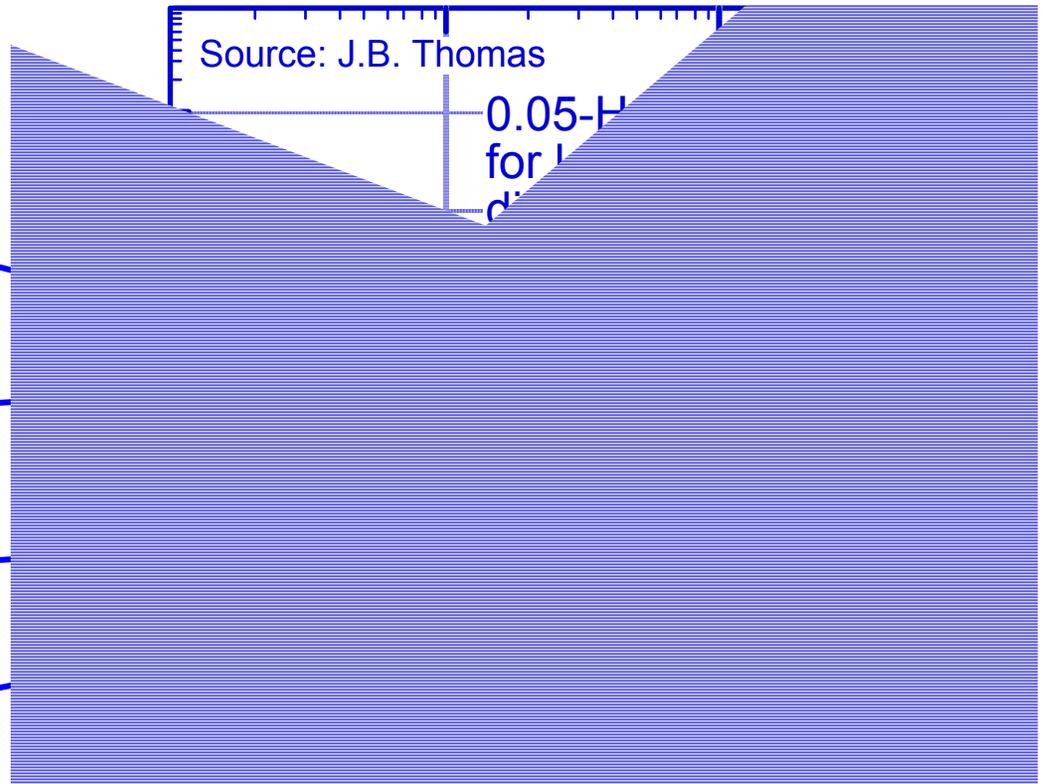
$$\left(\frac{\text{Microns}}{\text{sec}^2 \text{ Hz}^{1/2}} \right)$$

Accelerometer

USO sans GPS

USO with GPS

Microwave



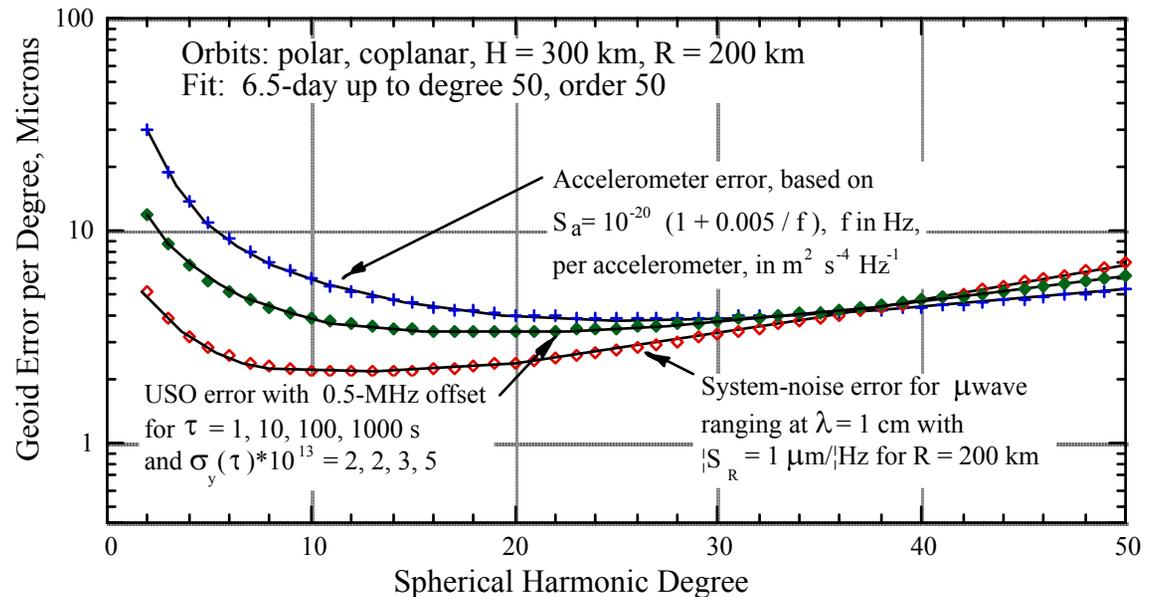
SOURCE: J.B. Thomas

Frequency, Hz

GRACE Mission

Limiting Errors Mapped to Geoid

The key to the long wavelength terms is the Accelerometer



The satellites must be mechanically quiet

- Avoid Parasitic Harmonic Oscillators
- No rotating machinery
- Limit Thrusting
- Heaters mounted on Low conductivity material - limit Lenz-Law effects
- Well staked cables

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French Electrostatic Accelerometer

70-gram Proof Mass

- 1x 4x 4-cm Titanium block
- Not caged

Electrostatic Suspension

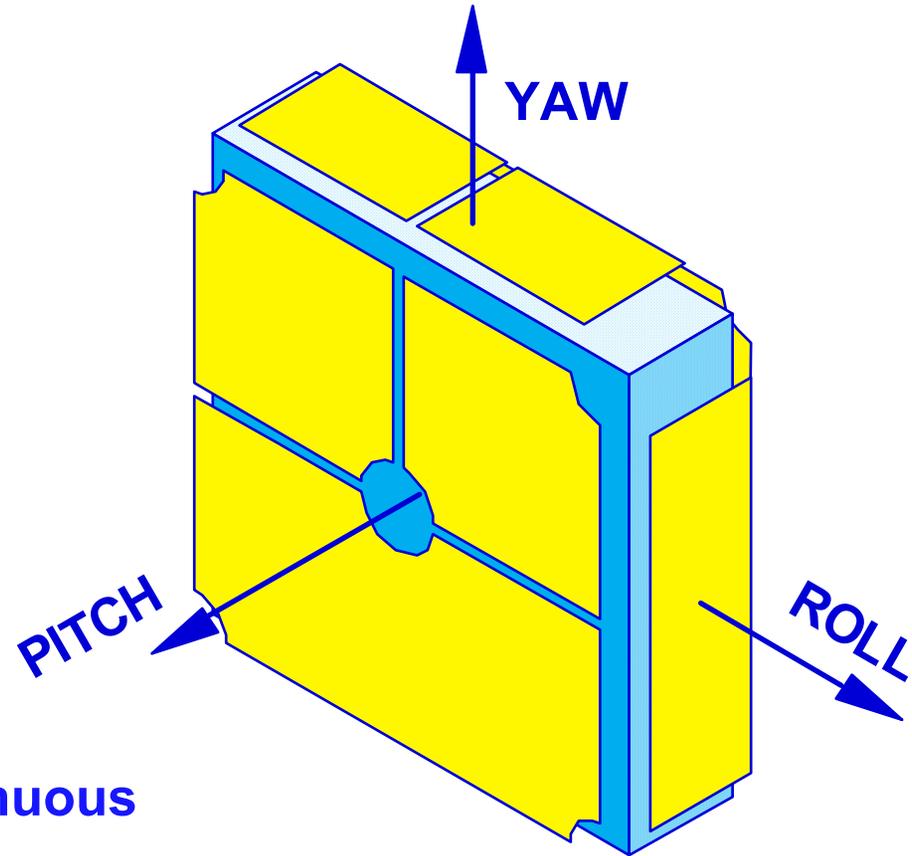
- 10-volt bias
- 150-micron gap
- 12-micron free motion

Performance

- Noise $10^{-10} \text{ m/s}^2 \text{ Hz}^{-1/2}$
- Full Scale $5 \times 10^{-5} \text{ m/s}^2$

Architectural Implication

- **No requirement for continuous drag compensation!**



Source: ONERA

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Non-Gravitational Effects

Non-Gravitational Forces

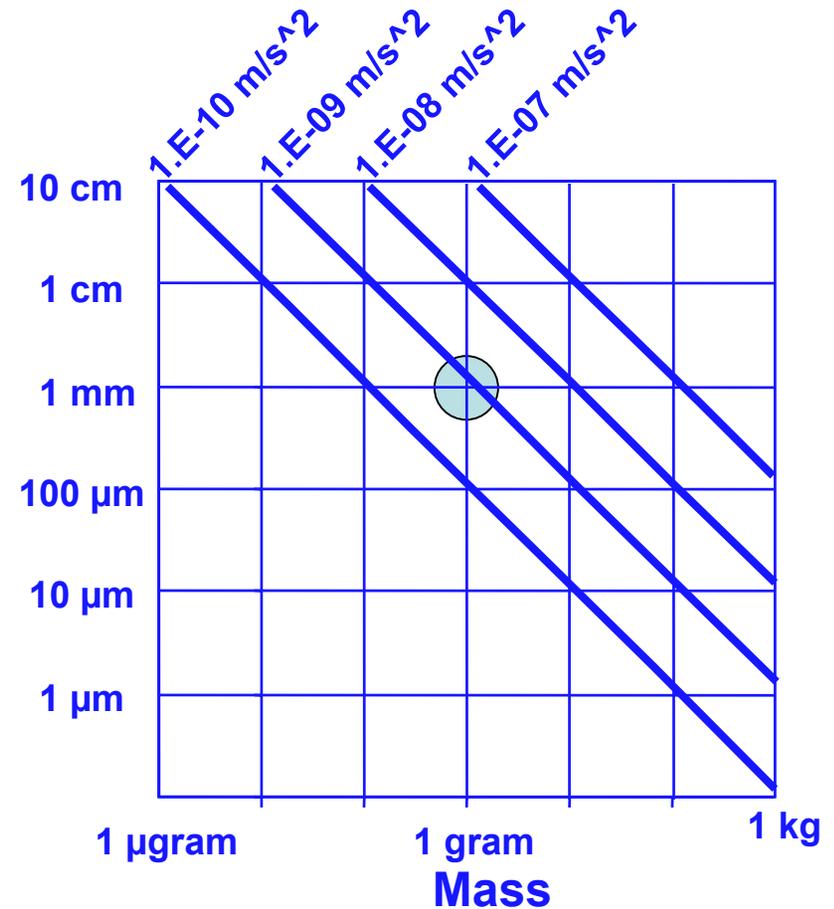
- Solar pressure = $50\text{E-}09 \text{ m/s}^2$
- Drag @ 500 km = $1\text{E-}07 \text{ m/s}^2$
- Drag @ 300 km = $5\text{E-}06 \text{ m/s}^2$

Parasitic Harmonic Oscillators

- @ frequency 0.1 Hz, 1-gram parasitic oscillator with amplitude of 1mm results in a satellite acceleration of $1\text{E-}09 \text{ m/s}^2$

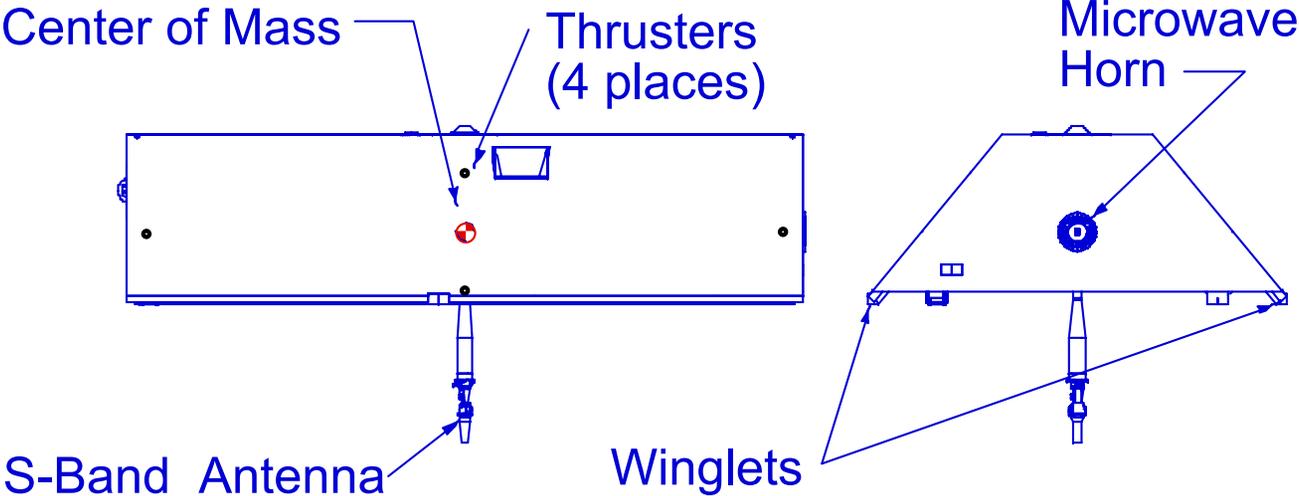
Rotating Machines

- Reaction wheel run at 600 to 3000 rpm
- This is 10 to 50 Hz
- Interferes with ACC control loops they have a resonance at $\sim 30 \text{ Hz}$



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Controlling Torques

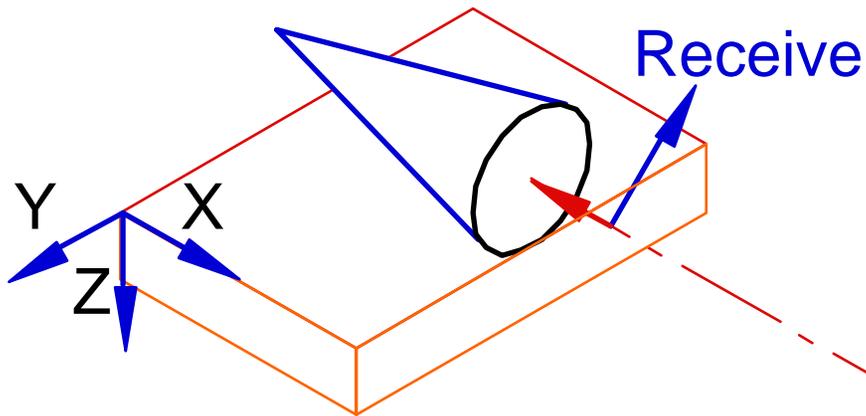


Side View

Front View

Astrium, GmbH

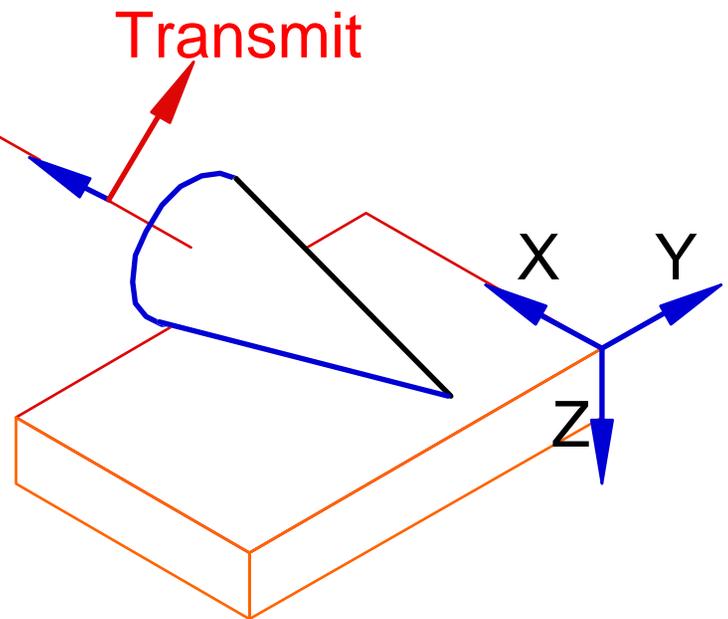
GRACE Mission K-Band Ranging



24- and 32-GHz
Unmodulated Carrier
Frequencies separated
by 670 kHz @ 32 GHz

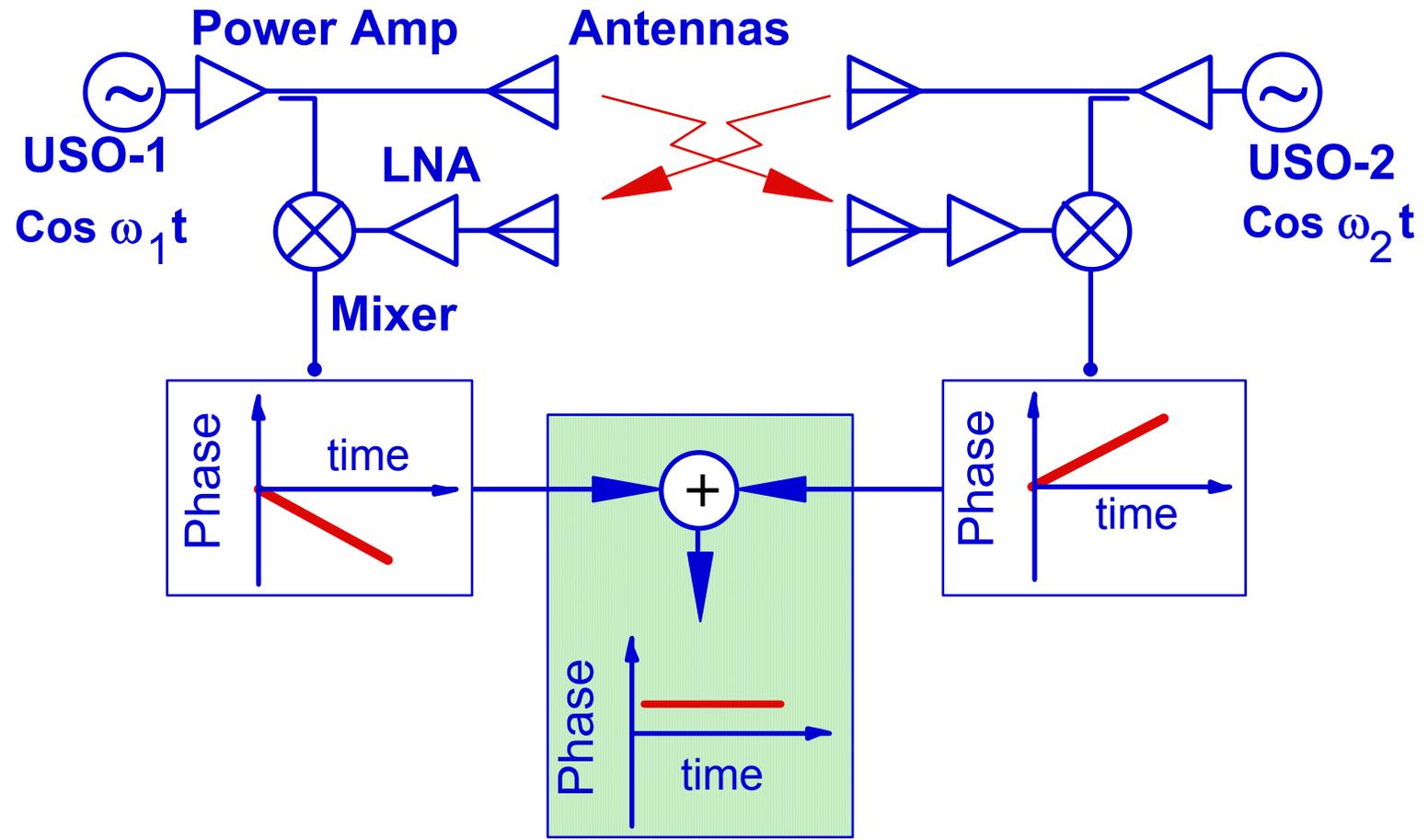
Transmit and Receive
Single Corrugated Horn
Linear Polarization
45° to Z-Axis

GRACE Satellites are twins



GRACE Mission Dual One-Way Ranging

$$\partial f/f = 10^{-13}$$



SOURCE: C.E. Dunn

The Laser Interferometer Option

Advantages

- The Transmit and Receive frequency are the same
 - Potential to Improve Ranging performance for the longest wave length terms

Microwave Offsets

- Lowered the offset between K-Band frequencies to under 1 MHz
 - Spitzmesser showed it could be done

Challenges in 1996

- Frequency stability $1E-12$ was not demonstrated
 - SIM was working on a cavity stabilization approach objective $1E-11$
- Needed arc-second level pointing to make fringes
 - An optical concept with less stringent pointing reqt had poor SNR

Abandoned after a 6 week preliminary design effort

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Risk Containment

Level of Integration into the I²PU

- GPS
- K-band Tone Tracking
- Timing Signals
- Star Camera Image Processing

Star Camera Configuration

Redundancy

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Level of IPU Integration

- | | |
|--|--|
| K-band Tone Tracking | <ul style="list-style-type: none">• Essential integration to achieve 100 psec time synchronization |
| Timing Signals
1-Hz OBDH | <ul style="list-style-type: none">• Synchronize telemetry and command with the instrumentation |
| Timing Signals
10-Hz ACC
1-MHz ACC | <ul style="list-style-type: none">• Required to synchronize the 10-Hz ACC data with the 10-Hz K-Band ranging data. Simplifies the digital filtering of the data by the Science Data System |
| Star Camera
Image
Processing | <ul style="list-style-type: none">• Intel 486 micro-processor from DTU Ęxpected similar problems to the 603e used in the BlackJack• Utility of K-band data depends on star camera data• Unit cost of Processors > \$250,000 (needed at least 4) |

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Star Camera Configuration

- **Two Star Cameras 45 degrees to Zenith - Camera pointed away from the Sun is "Prime" and used by AOCS.**
 - Simultaneous Sun and Moon blinding in both occurs monthly
 - Simply letting the satellite float with control actuators OFF works for 5- to 8-minute moon intrusions in the "prime camera"
 - Every 160 days, the sun shifts from one side of the satellite to the other. Prime camera must be switched at this point.
 - If one camera fails, the IMU provides an inertial reference during those periods when the Sun interferes with the only camera.
 - If the both the IMU and a camera fail on one Satellite, then leading satellite must switch places with the trailer
- **Three- & Four-camera options abandoned -**
 - Packaging close to the ACC was too difficult

GRACE Mission Cold Gas Sub-System

Center of Mass Stability

- CHAMP manifolds the two tanks together and has one high pressure regulator & 2 low pressure latch valves
- $1^{\circ}\text{K } \Delta T$ between Tanks moves the CoM $80 \mu\text{m}$

GRACE Dual-String Architecture

- No mass exchange between tanks from ΔT
- Redundant regulators
- Compensates for tuck-open thruster
- X-axis CoM is controlled by single string operation of orbit control maneuvers

